

WHAT IS CLAIMED IS:

1. A method of predistorting a complex baseband signal  $x$  having an in-phase component  $I$  and a quadrature component  $Q$ , said method comprising the steps of:

sampling the complex baseband signal  $x$  to obtain  $k$  samples  $I_k$  of the in-phase component and  $k$  samples  $Q_k$  of the quadrature component;

for each of the obtained samples determining a respective distortion factor  $D_k = \{(\tanh(Cx_k))/Cx_k\}e^{-jM_k}$ , where  $M_k = (Bx_k \tanh(Cx_k))/6$ ,  $x_k$  is the magnitude of the sample  $k$ , and  $C$  is a scaling factor;

multiplying each of the samples  $I_k$  of the in-phase component and each of the samples  $Q_k$  of the quadrature component by its respective distortion factor  $D_k$  to obtain a predistorted in-phase component sample and a predistorted quadrature component sample; and

combining the predistorted in-phase component samples and the predistorted quadrature component samples to provide a predistorted combined signal.

2. A method as claimed in claim 1, wherein for each of the  $k$  samples the respective distortion factor  $D_k$  is determined by:

determining the magnitude  $I_k$  of each of the  $k$  samples of the in-phase component and the magnitude  $Q_k$  of each of the  $k$  samples of the quadrature component;

for each of the  $k$  pairs of corresponding samples of the in-phase component and the quadrature component, determining a respective value of  $x_k = (I_k^2 + Q_k^2)^{1/2}$ ; and

for each value of  $x_k$ , determining a value of  $\tanh(Cx_k)$  and a value of  $(\tanh(Cx_k))/Cx_k$ .

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3. A method as claimed in claim 2, wherein for each value of  $x_k$  the value of  $\tanh(Cx_k)$  is determined from a lookup table.

4. A method as claimed in claim 2, wherein for each value of  $x_k$  the value of  $\operatorname{atanh}(Cx_k)/Cx_k$  is determined from a lookup table.

5. A method as claimed in claim 2, wherein for each of the  $k$  pairs of corresponding samples the respective value of  $x_k$  is determined by:

detecting the maximum value of  $I_k$  and  $Q_k$  by determining the larger of  $I_k$  and  $Q_k$ ;

detecting the minimum value of  $I_k$  and  $Q_k$  by determining the smaller of  $I_k$  and  $Q_k$ ;

calculating a value  $y_k = \frac{1}{2} \{(\text{the detected minimum value}) \div (\text{the detected maximum value})\}^2$ ; and

calculating a value of  $(I_k^2 + Q_k^2)^{1/2}$  as a function of  $y_k$ .

6. A method as claimed in claim 5, wherein the value of  $(I_k^2 + Q_k^2)$  is calculated as  $(\text{the detected maximum value}) \times \{(1 + y_k)/2 + \frac{1}{2} (1 + y_k - y_k^2 + y_k^3 - y_k^4 + y_k^5 - y_k^6)\}$ .

7. A method of generating an envelope predistorted radio frequency signal, said method comprising the steps of:

providing an envelope modulated signal including a complex baseband signal  $x$  having an in-phase component  $I$  and a quadrature component  $Q$ ;

sampling the complex baseband signal  $x$  to obtain  $k$  samples  $I_k$  of the in-phase component and  $k$  samples  $Q_k$  of the quadrature component;

for each of the obtained samples determining a respective distortion factor  $D_k = \{(\operatorname{atanh}(Cx_k))/Cx_k\}e^{-jM_k}$ , where  $M_k = (Bx_k \tanh(Cx_k))/6$ ,  $x_k$  is the magnitude of the sample  $k$ ,

and C is a scaling factor;

multiplying each of the samples  $I_k$  of the in-phase component and each of the samples  $Q_k$  of the quadrature component by its respective distortion factor  $D_k$  to obtain a predistorted in-phase component sample and a predistorted quadrature component sample;

combining the predistorted in-phase component samples and the predistorted quadrature component samples to provide a predistorted combined signal;

up-converting the predistorted combined signal to provide a radio frequency signal;

and

applying the radio frequency signal to a power amplifier have hyperbolic tangent distortion.

8. A method as claimed in claim 7, wherein for each of the k samples the respective distortion factor  $D_k$  is determined by:

determining the magnitude  $I_k$  of each of the k samples of the in-phase component and the magnitude  $Q_k$  of each of the k samples of the quadrature component;

for each of the k pairs of corresponding samples of the in-phase component and the quadrature component, determining a respective value of  $x_k = (I_k^2 + Q_k^2)^{1/2}$ ; and

for each value of  $x_k$ , determining a value of  $\tanh(Cx_k)$  and a value of  $(\tanh(Cx_k))/Cx_k$ .

9. A method as claimed in claim 8, wherein for each value of  $x_k$  the value of  $\tanh(Cx_k)$  is determined from a lookup table.

10. A method as claimed in claim 8, wherein for each value of the  $x_k$  the value of  $\tanh(Cx_k)/x_k$  is determined from a lookup table.

11. A method as claimed in claim 8, wherein for each of the  $k$  pairs of corresponding samples the respective value of  $x_k$  is determined by:

- detecting the maximum value of  $I_k$  and  $Q_k$  by determining the larger of  $I_k$  and  $Q_k$ ;
- detecting the minimum value of  $I_k$  and  $Q_k$  by determining the smaller of  $I_k$  and  $Q_k$ ;
- calculating a value  $y_k = \frac{1}{2} \{(\text{the detected minimum value}) \div (\text{the detected maximum value})\}^2$ ;
- calculating a value of  $(I_k^2 + Q_k^2)^{\frac{1}{2}}$  as a function of  $y_k$ .

12. A method as claimed in claim 11, wherein the value of  $(I_k^2 + Q_k^2)$  is calculated as  $(\text{the detected maximum value}) \times \{(1 + y_k)/2 + \frac{1}{2} (1 + y_k - y_k^2 + y_k^3 - y_k^4 + y_k^5 - y_k^6)\}$ .

13. A method as claimed in claim 7, further comprising the step of:

transmitting the radio frequency signal.

14. A method as claimed in claim 7, wherein the scaling factor  $C$  is based on a comparison of the envelope of the complex baseband signal  $x$  and the envelope of the radio frequency signal.

15. Apparatus for predistorting a complex baseband signal  $x$  having an in-phase component  $I$  and a quadrature component  $Q$ , said apparatus comprising:

a sampling circuit for sampling the complex baseband signal  $x$  to provide  $k$  samples  $I_k$  of the in-phase component and  $k$  samples  $Q_k$  of the quadrature component;

a distortion determining circuit for determining for each of the provided samples a respective distortion factor  $D_k = \{(\tanh(Cx_k))/Cx_k\}e^{-jM_k}$ , where  $M_k = (Bx_k \tanh(Cx_k))/6$ ,  $x_k$  is the magnitude of the sample  $k$ , and  $C$  is a scaling factor;

a first multiplier for multiplying each of the samples  $I_k$  of the in-phase component and each of the samples  $Q_k$  of the quadrature component by its respective distortion factor  $D_k$  to obtain a predistorted in-phase component sample and a predistorted quadrature component sample; and

a summing circuit for combining the predistorted in-phase component samples and the predistorted quadrature component samples to provide a predistorted combined signal.

16. Apparatus as claimed in claim 15, wherein said distortion determining circuit comprises:

a first calculation circuit for determining for each of the  $k$  pairs of corresponding samples of the in-phase component and the quadrature component, a respective value of  $x_k = (I_k^2 + Q_k^2)^{1/2}$ ; and

a second calculation circuit for determining for each value of  $x_k$  a value of  $\tanh(Cx_k)$  and a value of  $(\tanh(Cx_k))/Cx_k$ .

17. Apparatus as claimed in claim 16, wherein said second calculation circuit includes a plurality of lookup tables.

18. Apparatus as claimed in claim 16, wherein said first calculation circuit comprises:

first means for detecting the maximum value of  $I_k$  and  $Q_k$  by determining the larger of  $I_k$  and  $Q_k$ ;

second means for detecting the minimum value of  $I_k$  and  $Q_k$  by determining the smaller of  $I_k$  and  $Q_k$ ;

third means for calculating a value of  $y_k = \frac{1}{2} \{(\text{the detected minimum value}) \div (\text{the detected maximum value})\}^2$ ; and

fourth means for calculating a value if  $(I_k^2 + Q_k^2)^{1/2}$  as a function of  $y_k$ .

19. Apparatus as claimed in claim 16, wherein said first calculating circuit calculates the value of  $(I_k^2 + Q_k^2)^{1/2}$  as (the detected maximum value)  $\times \{(1 + y_k)/2 + \frac{1}{2}(1 + y_k - y_k^2 + y_k^3 - y_k^4 + y_k^5 - y_k^6)\}$ .

20. Apparatus as claimed in claim 15, wherein said sampling circuit, said distortion determining circuit, said first and second multipliers, and said summing circuit comprise a gate array.

21. Apparatus as claimed in claim 20, wherein said gate array is a field programmable gate array.

22. Apparatus for generating an envelope predistorted radio frequency signal, said apparatus comprising:

a source of an envelope modulated signal including a complex baseband signal  $x$  having an in-phase component  $I$  and a quadrature component  $Q$ ;

a sampling circuit for sampling the baseband signal  $x$  to provide  $k$  samples  $I_k$  of the in-phase component and  $k$  samples  $Q_k$  of the quadrature component;

a distortion determining circuit for determining for each of the provided samples a respective distortion factor  $D_k = \{(\tanh(Cx_k))/Cx_k\}e^{-jM_k}$ , where  $M_k = (Bx_k \tanh(Cx_k))/6$ ,  $x_k$  is the magnitude of the sample  $k$ , and  $C$  is a scaling factor;

a first multiplier for multiplying each of the samples  $I_k$  of the in-phase component and each of the samples  $Q_k$  of the quadrature component by its respective distortion factor  $D_k$  to obtain a predistorted in-phase component sample and a predistorted quadrature component sample;

a summing circuit for combining the predistorted in-phase component samples and the predistorted quadrature component samples to provide a predistorted combined signal;

an up-converter for up-converting the predistorted combined signal to provide a radio frequency signal; and

a power amplifier having hyperbolic tangent distortion for amplifying the radio frequency signal while canceling the predistortion therein.

23. Apparatus as claimed in claim 22, wherein said distortion determining circuit comprises:

a first calculation circuit for determining for each of the  $k$  pairs of corresponding samples of the in-phase component and the quadrature component, a respective value of  $x_k = (I_k^2 + Q_k^2)^{1/2}$ ; and

a second calculation circuit for determining for each value of  $x_k$  a value of  $(\tanh(Cx_k))$  and a value of  $\text{atanh}(Cx_k)/Cx_k$ .

24. Apparatus as claimed in claim 23, wherein said second calculation circuit includes a plurality of lookup table.

25. Apparatus as claimed in claim 23, wherein said first calculation circuit comprises:

first means for detecting the maximum value of  $I_k$  and  $Q_k$  by determining the larger of  $I_k$  and  $Q_k$ ;

second means for detecting the minimum value of  $I_k$  and  $Q_k$  by determining the smaller of  $I_k$  and  $Q_k$ ;

third means for calculating a value of  $y_k = \frac{1}{2} \{(\text{the detected minimum value}) + (\text{the detected maximum value})\}^2$ ; and

fourth means for calculating a value of  $(I_k^2 + Q_k^2)^{1/2}$  as a function of  $y_k$ .

26. Apparatus as claimed in claim 23, wherein said first calculation circuit calculates the value of  $(I_k^2 + Q_k^2)^{1/2}$  as (the detected maximum value)  $\times \{(1 + y_k)/2 + \frac{1}{2}(1 + y_k - y_k^2 + y_k^3 - y_k^4 + y_k^5 - y_k^6)\}$ .

27. Apparatus as claimed in claim 22, wherein said sampling circuit, said distortion determining circuit, said first and second multipliers, and said summing circuit comprise a gate array.

28. Apparatus as claimed in claim 27, wherein said gate array is a field programmable gate array.

29. Apparatus as claimed in claim 22, further comprising a circuit for providing the scaling factor C based on a comparison of the envelope of the complex baseband signal  $x$  and the envelope of the radio frequency signal.

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